Pushing extreme ultraviolet lithography development beyond 22 nm half pitch

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Microfield exposure tools (METs) have and continue to play a dominant role in the development of extreme ultraviolet resists and masks. One of these tools is the SEMATECH Berkeley 0.3 numerical aperture (NA) MET. Here, the authors investigate the possibilities and limitations of using the 0.3 NA MET for sub-22-nm half-pitch development. They consider mask resolution limitations and present a method unique to the centrally obscured MET, allowing mask patterning resolution limitations to be overcome. The method, however, comes at the cost of increased sensitivity to mask surface roughness. They also explore projection optics resolution limits and describe various illumination schemes allowing resolution enhancement. At 0.3 NA, the 0.5 $k_1$ factor resolution limit is 22.5 nm, meaning that conventional illumination is of limited utility for sub-22-nm development. In general, resolution enhancing illumination encompasses increased coherence. They study the effect of this increased coherence on line-edge roughness (LER), which, along with resolution, is another crucial factor in sub-22-nm resist development. Due to coherence induced LER limitations, addressing the development at 16 nm half pitch and beyond will ultimately require higher NA systems. © 2009 American Vacuum Society. [DOI: 10.1116/1.3237092]

I. INTRODUCTION

Despite the recent availability of full field extreme ultraviolet (EUV) alpha tools,1,2 microfield exposure systems3–5 continue to play a crucial role in the development of EUV lithography. This is especially true now that advanced development has started to focus on sub-22-nm half-pitch resolution. Figure 1 shows Prolith6 modeling results of the limits of a tool with a numerical aperture (NA) of 0.25 and conventional disk illumination with a coherence factor ($\sigma$) of 0.5. Note that coherent light corresponds to $\sigma$ of 0 and incoherent light to $\sigma$ of infinity. At $\sigma$ of 0.5, the illumination coherence width is twice as large as the diffraction-limited resolution of the lithographic optics. Moreover, we have assumed 7% effective flare and 1 nm of aberrations randomly distributed over Zernikes 5–37. We note that Zernikes 1–4 are piston, $x$ tilt, $y$ tilt, and defocus, respectively. Taking the resolution limit to correspond to a contrast of 50%, the modeling results predict a resolution limit of 27 nm half pitch, which correlates well with published experimental results.7 Evidently, sub-22-nm half-pitch development is not feasible with such tools.

Considering instead 0.3 NA microfield tools, modeling results show similar limitations when utilizing conventional illumination. Figure 2 shows the aerial-image contrast as a function of half pitch for the SEMATECH Berkeley microfield exposure tool (BMET) with annular illumination illumination ($0.35<\sigma<0.55$). Flare and wavefront aberration values are taken from the literature.8,9 Here, we find the 50% contrast resolution limit to be 22 nm. Even at 0.3 NA it is not
possible to enter the sub-22-nm regime using conventional illumination and masks. A significant benefit of the BMET, however, is that it enables lossless variable illumination, allowing resolution enhancement to be implemented. Figure 3 shows the aerial-image modeling results for four different resolution enhancing illumination settings. In all cases, vertical lines and spaces are modeled, but we note that the two 45°-rotated dipoles are capable of imaging Manhattan geometry (both horizontal and vertical lines). For the x-oriented dipole cases, only vertical line resolution is enhanced and the system suffers from forbidden pitches due to the central obscuration in the projection optics. Based on the 50% aerial-image contrast criterion, all cases support sub-22-nm half-pitch resolution with the most aggressive case supporting 12 nm half pitch.

Fig. 1. Aerial-image contrast modeling results for an EUV tool with 0.25 NA and conventional disk illumination with coherence factor ($\sigma$) of 0.5. Optical parameters are set to 7% effective flare and 1 nm wavefront aberrations randomly distributed over Zernikes 5–37. Zernikes 1–4 are piston, $x$ tilt, $y$ tilt, and defocus, respectively.

Fig. 2. Aerial-image contrast as a function of half pitch for the SEMATECH BMET with annular illumination illumination (0.35<$\sigma$<0.55). Flare and wavefront aberration values are taken from the literature (Refs. 8 and 9).

Fig. 3. Aerial-image modeling results for four different resolution enhancing illumination settings in the BMET. In all cases, vertical lines and spaces are modeled; however, the two 45°-rotated dipoles are capable of imaging Manhattan geometry (both horizontal and vertical lines).

Fig. 4. Direct comparison of printing (top row) and modeling (bottom row) results for radial gratings of varying half pitch using 45°-rotated dipole illumination with a pole radius of 0.15 and an offset of 0.57. The orientation and pitch dependence of the imaging performance are clear and correlate well between modeling and experiment.
II. DEMONSTRATION OF RESOLUTION ENHANCING ILLUMINATION

It is evident that the ability to control illumination conditions is crucial to the attainment of sub-22-nm resolution in current EUV tools. Figure 4 demonstrates that illumination control in the BMET is indeed possible and the results are predictable. Shown is the direct comparison of printing and modeling results for radial gratings of varying half pitch using 45°-rotated dipole illumination with a pole radius of 0.15 and an offset of 0.57. The orientation and pitch dependence of the imaging performance are clear and correlate well between modeling and experiment. Having confidence in the illumination control, we further use the 45°-rotated dipole to print vertical lines and spaces, as shown in Fig. 5. Good printing performance is seen down to 20 nm. Next, we consider x-oriented dipole illumination (Fig. 6). Despite the significantly improved expected aerial image, we again see a resolution limit in resist of approximately 20 nm.

The above results raise the question about the mask: could the mask also be contributing to the observed resolution limit? Figure 7 shows scanning electron micrographs from the EUV reticle used on the BMET demonstrating that the mask itself also suffers from a limit of approximately 20 nm. We note that similar results have been found on masks from other suppliers.

III. GETTING AROUND MASK RESOLUTION LIMITS

Mask resolution limitations can be significantly mitigated through a process we refer to as pseudostrong phase shift mask. In strong phase shift mask technology, the zeroth diffraction order from the object is suppressed by virtue of destructive interference, which, in turn, leads to the printed pitch being one-half of the patterned pitch on the mask (in addition to the normal system demagnification). Strong phase shift mask technology, however, is not readily available at EUV due to the complex mask fabrication process. Nevertheless, with a centrally obscured optic, the same effect of zeroth order suppression can be achieved by ensuring that the pupil fill is completely blocked by the obscuration (Fig. 8). The zeroth order transmitted by the conventional binary amplitude mask being restricted in the pupil to the actual area of the illumination pupil fill will be blocked. This leads to an image plane electric field that is essentially indistinguishable from that would have appeared had a strong phase shift mask been used. The ultimate resolution limit of this method is identical to the extreme dipole case, or approximately 12 nm half pitch for the BMET design; however, the mask pitch is relaxed by a factor of 2.

Figure 9 shows printing results in the pseudostrong phase shift mask mode. On-axis disk illumination with a coherence factor of 0.15 was used. Note that the BMET central obscuration is 30% of the full pupil in radius. The printing results again show a resolution limit of approximately 20 nm, suggesting that the resist is indeed the limiting factor.

IV. MASK ROUGHNESS LIMITATIONS

For both the resolution enhanced illumination and pseudostrong phase shift mask cases, low sigma high coherence illumination is required. It has been shown, however, that
such illumination conditions render the process significantly more susceptible to multilayer-roughness induced phase variations on the mask.\textsuperscript{10–13} Thus modeling is used to study the potential importance of these effects to the pseudostrong phase shift mask results presented here. For details on the modeling procedure and the mask metrology performed to determine the mask characteristics, the reader is referred to Ref. 12. Figure 10 shows aerial-image results as well as thresholded versions demonstrating the strong impact of mask effects on the line-edge roughness (LER). Note that the thresholded aerial image corresponds to the response of an ideal resist process. These results show that the mask, in addition to the resist, leads to printing limitations in the sub-22-nm regime.

V. SUMMARY

Achieving sub-22-nm half-pitch resolution with current of 0.25 and 0.3 NA EUV tools requires the use of modified illumination or other resolution enhancement methods. The BMET has been used to demonstrate sub-22-nm printing with both modified illumination and a spatial filtering method akin to strong phase shift mask technology yet compatible with conventional binary amplitude masks. These techniques, however, all rely on high spatial coherence which appears to give rise to unacceptably large mask-induced LER effects. Ultimately, to address development at the 16 nm half-pitch node, higher NA systems are required.

To address the 16 nm development need, SEMATECH has launched a program to develop 0.5 NA microfield exposure tools\textsuperscript{14} with the goal of installing one of those tools at Lawrence Berkeley National Laboratory’s Advanced Light Source synchrotron facility, enabling the modified illumination discussed above at this even higher NA. Such illumination capabilities would allow this new tool to achieve resolution limits below 8 nm. Figure 11 shows a schematic of the 0.5 NA optical design which as with the 0.3 NA MET will be a centrally obscured, two-element Schwarzschild-type optic. Also shown in Fig. 11 are the aerial-image modeling results for three different illumination conditions.

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